# B.E. (C. E.) $4^{\text {th }}$ Semester Final Examination, 2010 HYDRAULICS II (AM 402) <br> Time: 3 hrs. Full Marks: 70 <br> <br> Attempt SIX questions taking ANY THREE from each half <br> <br> Attempt SIX questions taking ANY THREE from each half All questions cany equal marks 

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## FIRST HALF

Q. 1. a) A model with a scale of $1 / 10$ is constructed for an impulse turbine to develop 7350 KW power under a net head of 9 m while running at 100 rpm . If the efficiency of the actual turbine is $88 \%$ and the head available in the test house is 6 m , find
i) Running speed of the model, ii) Flow rate required in the test house, iii) Power developed by the model and iv) Specific speed of the model and the actual turbine.
b) Find the permissible height of setting a Francis water turbine above the tailrace level using following data:
Power to be developed $=3.75$ MW under a head of 100 m .
The generator coupled with the shaft has 12 poles with frequency 50 cycles/sec.
Local atmospheric pressure $=9.75 \mathrm{~m}$ and vapor pressure head $=0.43 \mathrm{~m}$.
Q. 2. a) Prove that the specific speed of a reaction turbine can be expressed as
$\mathrm{N}_{s}=576.33 \mathrm{~K}_{\mathrm{u}}\left(\mathrm{D}_{2} / \mathrm{D},\right) \mathrm{V}\left(\mathrm{r} \mid, \backslash /{ }_{2} \mathrm{~K}_{2}\right)$, where,
K, , $=$ Speed ratio, $\mathrm{D}_{2}=$ Outlet diameter, $\mathrm{Dj}=$ Inlet diameter, = Blockage factor at outlet due to the vane thickness and $y_{2}=$ Flow ratio at the outlet.
b) A nozzle having a velocity coefficient of 0.98 discharges a 15 cm diameter water jet under a head of 275 m . Take ct $\mid=0^{\circ}, 0=165^{\circ}$, speed ratio $=0.46$, wheel diameter $=2.44 \mathrm{~m}$, mechanical efficiency $=97 \%$ and head loss in bucket surface friction as 0.5 $\mathrm{V}_{\mathrm{r} 2}{ }^{2} / 2 \mathrm{~g}$ where $\mathrm{V}_{\mathrm{r} 2}$ is the relative velocity at the outlet. Find i) absolute velocity of water at outlet ii) power carried away in the water discharged from the buckets ii) power lost in bucket friction iv) hydraulic efficiency and v) overall efficiency.
Q. 3. The inner diameter of an inward flow reaction turbine is 0.65 times the outer diameter. The turbine has a wheel 0.6 m diameter and 5 cm wide at the outer rim. The velocity of flow is uniform throughout the wheel and the wheel blade angles at the inlet and outlet are 95" and 14" respectively and $8 \%$ of the circumferential area is blocked by blade thickness. The head on the turbine is 53.6 m , the hydraulic efficiency $88 \%$, the overall efficiency $81 \%$ and the discharge at the outlet of the runner is radial. ric\}<Tw'i«e $\wedge_{\vee} \%^{*}$ av><! cwij>t*t $\mathrm{j}-\mathrm{n}^{\wedge} \mathrm{o}$ <? $\mathrm{Xii}_{u}-\mathrm{Im} \boldsymbol{V},{ }_{\mathrm{n}} \boldsymbol{i}$ Q. 4. A centrifugal pump having 4 stages in parallel delivers 180 litres $/ \mathrm{sec}$ of liquid against a head of 25 m , the diameter of the impeller being 22.5 cm and speed $1700 \mathrm{rev} / \mathrm{min}$. A pump is to be-made up with a number of identical stages in series each stage being similar to those as in the first pump, to run at $1250 \mathrm{rev} / \mathrm{min}$ and to deliver approximately 240 litres $/ \mathrm{sec}$ against a head of 250 m . Find the number of stages, diameter of impeller and actual discharge.
Q. 5. a) What is the use of DRAFT tube in reaction turbine?
b) The head available in a vertical shaft Francis turbine is 50 m and the runner speed is 380 $\mathrm{rev} / \mathrm{min}$. The inlet of the turbine runner is placed 1.8 m above the tailrace level and the area and diameter of the runner at the inlet are $0.24 \mathrm{~m}^{2}$ and I m respectively. The guide and runner vane angle at the inlet are $20^{\circ}$ and $120^{\circ}$ respectively. The wnter enters a draft tube without whirl 1.6 m above the tail race level and the draft tube dia there is 56 cm . \# outlet the draft tube is 72 cm diameter. If the frictional losses in the runner amount to 3 m and in the draft tube 1.5 m and the overall efficiency $=0.9 \mathrm{x}$ hydraulic efficiency, find a) brake power of the turbine b) hydraulic efficiency c) pressure head at the inlet to the runner d) pressure head at the entry to the draft tube. Assume head loss in guide passage $0 .!5 \mathrm{~m}$.

## SECOND HALF

[6], (a) Water from a reservoir flows through a pipe of length $\boldsymbol{I}$ and diameter $\boldsymbol{D}$ and discharges through a nozzle of tip diameter $\boldsymbol{d}$. The loss of head in the nozzle is $\boldsymbol{k} \boldsymbol{V} / \mathbf{2} \boldsymbol{g}$ where $\boldsymbol{k}$ is constant and $\boldsymbol{V}$ is the velocity at the nozzle exit. If f is the friction factor for the pipe, show that for the maximum power of jet $(\boldsymbol{d} / \boldsymbol{D})=\left[\left\{\left(\begin{array}{ll}1 & +\boldsymbol{k}) \\ \mathrm{D}\end{array}\right\} /(2 . / \mathrm{L})\right]^{0}{ }^{25}\right.$. (6)
(b) 200 KW is to be transmitted through a 10 km long water pipe, the head at inlet of the pipe being 500 m . If/- $0.03, \quad \quad^{\wedge} \mathbf{B}$ the minimum diameter of the pipetb $\mathbf{W} \mathrm{y}^{*} \mathrm{~T}>^{\wedge}$
[7]. 30 mVs of water is to be pumped for 14 hours a day to supply a township. The supply is carried through two identical pipes, each 12 km long, connected in parallel. The annual cost of each pipe line, in rupees, is $2.5 \times 10^{5} \boldsymbol{D} \sim$, where $\boldsymbol{D}$ is the pipe diameter in meters. The pumps are operated by electric motors and the overall efficiency of the pumps and motor units is $75 \%$. The cost of electric energy supplied to the motors is 125paisa per KWH. The friction factor for the pipe is 0.02 . Calculate the economic diameter of the pipes.
[8]. (a) Derive Chezy equation for steady uniform flow in an open channel.
(b) A trapezoidal channel is required to carry 6 mVs of water at a velocity of $1.5 \mathrm{~m} / \mathrm{s}$. Find the' most economical cross-section if the channel has side slopes of 1 vertical to 2 horizontal. Fur the same discharge what saving in power would result if this trapezoidal section is replaced by a rectangular section 1.5 m deep and 3 m wide? Use $\mathrm{C}=55 \mathrm{~m}^{12} / \mathrm{s}$ in Chezy formula.
[9]. (a) Water flows at a rate of $1 \mathrm{~m}^{3} / \mathrm{s}$ along a channel of rectangular section 1.6 m in width. Calculate the critical depth. If a standing wave occurs at a point where the upstream depth is 0.25 m , what would be the rise in water level produced and power lost in the standing wave. (5) (b) A rectangular channel 2.4 m wide carries a uniform flow of 7 m 7 s at a depth of 1.5 m . If there is alocal rise of 0.15 m in the bed level, calculate the change in water surface elevation. What can be the maximum rise in the bed elevation such that the upstream depth is not affected?
[10]. (a) Define and explain the following terms- alternate depth, conjugate depth and specific energy
(b) The spectflc^ener $\mathrm{r}^{\wedge \wedge} \mathrm{a}^{\wedge}$ a section of a 4 m wide rectangular channel, conveying a discharge of 12 mVs is $2 \mathrm{~m} . \quad \wedge \mathrm{t} £ \mathrm{e}$ two possible flow depths.
( c) A rectangular channel 5 m wide conveys a discharge of $15 \mathrm{~m}^{3} / \mathrm{s}$ of water at a depth of 2 m . If the width of the channel is reduced to 3.5 m on the downstream side, will the water surface in the channel be disturbed in the upstream? What will be the depth of flow in the reduced section? (5)

